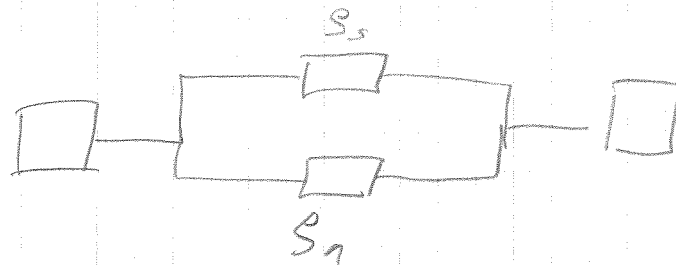


The two fluid model

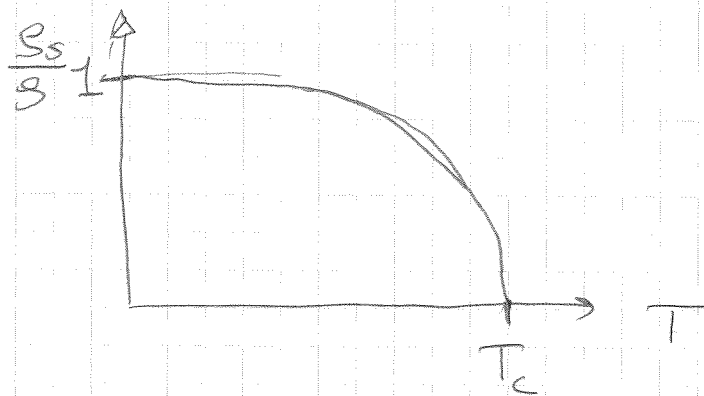
$$S = S_s + S_n$$

S_s	S_n
"Superelectrons"	Normal electrons
No scattering	scattering
No entropy	Entropy
Infinite conductance	Normal conductance

BCS: Cooper pairs



$$R \ll 0 \quad T < T_c$$

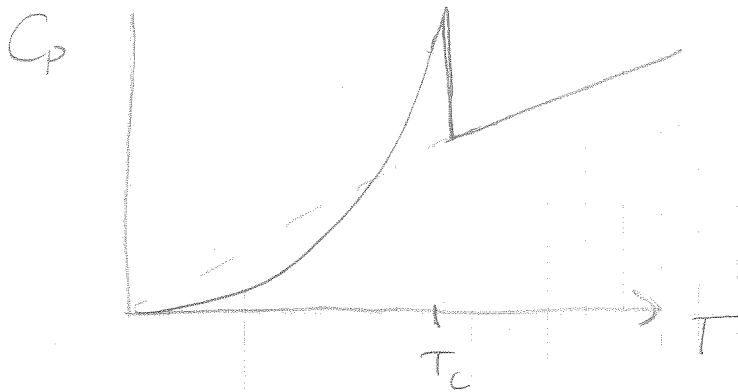


$T=0$ $\mathcal{R} \propto S_n$ i.e. very small
since S_s carries no entropy

$$|\psi\rangle = \sqrt{n_s} \cdot e^{i\theta}$$

n_s can be thought of as the electrons that form Cooper-pairs
The super current is given by

$$\vec{J}_s = -n_s e \vec{v}_s$$



From the thermal properties

$$n_s \sim n \left(1 - \left(\frac{T}{T_c}\right)^4\right)$$

High frequency conductivity of SC

$$\sigma = \sigma_n + \sigma_s$$

$$\vec{J}_s = -\sigma_s e \vec{v}_s$$

$$\vec{J}_n = -\sigma_n e \langle \vec{v}_n \rangle$$

Normal electrons

$$m \cdot \frac{d\langle v_n \rangle}{dt} + m \cdot \frac{\langle v_n \rangle}{\tau} = \vec{F} = -e\vec{E}$$

$$\tau \sim 10^{-13} \text{ s}$$

if variations in \vec{E} are slow on this time scale

$$\frac{m \langle \vec{v}_n \rangle}{\tau} = -e\vec{E}$$

$$\vec{J}_n = -\sigma_n e \langle \vec{v}_n \rangle = -\sigma_n e \left(-\frac{e\tau}{m} \right) \vec{E}$$

$$\vec{J}_n = \sigma_n \vec{E} \Rightarrow$$

$$\sigma_n = \frac{\sigma_n e^2 \tau}{m}$$

Super electrons

$$m \frac{d\vec{v}_s}{dt} = -e\vec{E}$$

assume $\vec{E} = \vec{E}_0 e^{j\omega t} \Rightarrow$

$$\vec{v}_s = -\frac{e}{m} \frac{\vec{E}_0}{j\omega} e^{j\omega t}$$

$$\vec{J}_s = -g_s e \vec{V}_s = -g_s e \frac{e}{m} \frac{1}{j\omega} \vec{E} = \sigma_s \vec{E}$$

$$\sigma_s = g_s \frac{e^2}{m} \frac{1}{j\omega} = -j g_s \frac{e^2 \tau}{m} \frac{1}{\omega \tau}$$

$$\vec{J} = \vec{J}_n + \vec{J}_s = (\sigma_n - j\sigma_s) \vec{E}$$

$$\sigma_n = g_n \frac{e^2 \tau}{m} \quad \sigma_s = g_s \frac{e^2}{m} \frac{1}{\omega}$$

i.e. real part dep. on g_n
 imagin. part dep. on g_s

$$\omega \tau \ll 1$$

$$f < 10 \text{ GHz}$$

$$\sigma_s = \frac{1}{\omega L} \Rightarrow L = \frac{m g_s}{e^2}$$



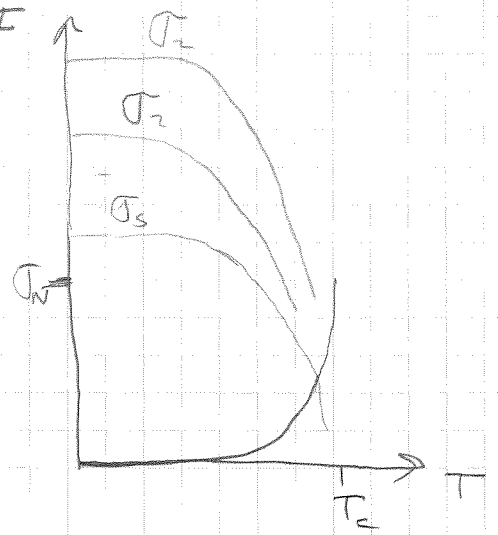
$$\sigma_n = g_n \frac{e^2 \tau}{m}$$

$$\sigma_{\text{tot}} = g_n \frac{e^2 \tau}{m} - j g_s \frac{e^2 \tau}{m} \frac{1}{\omega \tau}$$

$$\sigma_n = g_n \frac{e^2 \tau}{m}$$

$$\sigma_{\text{tot}} = \left(\frac{g_n}{g} - j \frac{g_s}{g} \frac{1}{\omega \tau} \right) \sigma_n$$

$$\frac{\sigma_{\text{tot}}}{\sigma_n} = \frac{g_n}{g_s} \omega \tau \ll 1$$



Dissipated power per unit volume

$$\frac{P}{V} = \rho \cdot J^2 = \operatorname{Re}\left(\frac{1}{\sigma}\right) J^2 = \frac{\sigma_1}{\sigma_1^2 + \sigma_2^2} J^2 \approx \frac{\sigma_1}{\sigma_2^2} J^2$$

$$\left[\frac{1}{\sigma_1 - j\sigma_2} = \frac{\sigma_1 + j\sigma_2}{\sigma_1^2 + \sigma_2^2} \right]$$

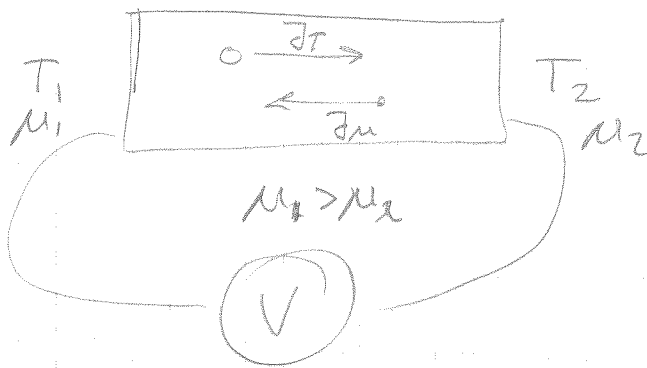
$$\frac{\sigma_1}{\sigma_2^2} \propto \omega^2$$

at 100 GHz SC no better than N

The thermoelectric effect

Normal Metal

$$T_1 > T_2$$

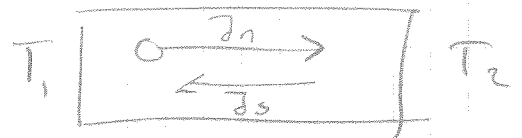


Flow of e from hot to cold gives rise to an electrochemical potential which drives current in the opposite direction leading to a net zero current

$$\vec{J} = \vec{J}_T + \vec{J}_n = 0$$

 Seebeck effect

SC



$$\vec{J} = \vec{J}_n + \vec{J}_s = 0$$

In a SC no potential difference can develop

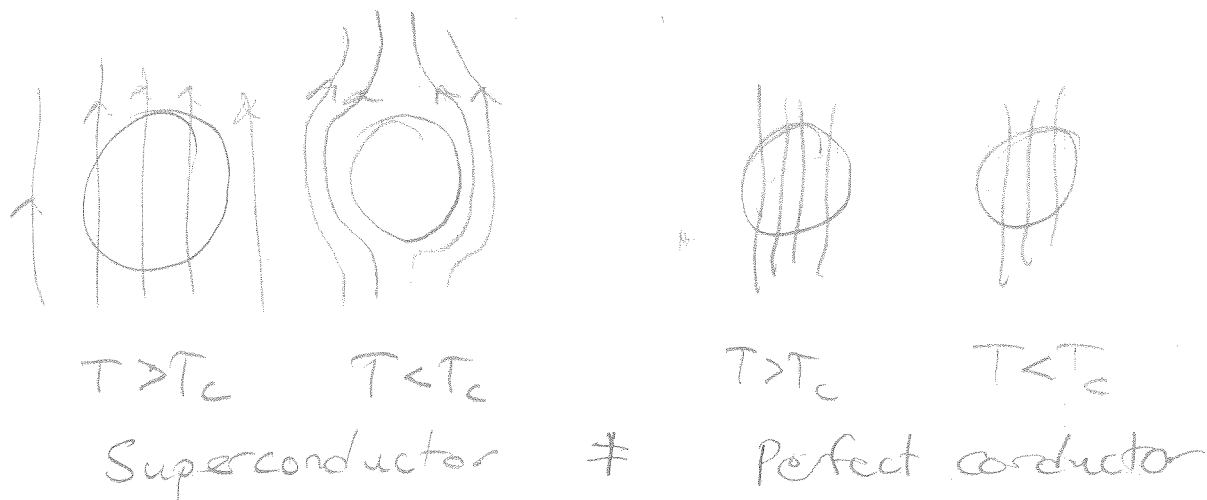
$$\vec{J}_s$$
 exactly cancels
$$\vec{J}_n$$

$$\vec{J} = \vec{J}_n + \vec{J}_s = 0$$

 No Seebeck effect

This can be used to measure the seebeck coefficient of a single metal

The Meissner effect



Something more

$R=0$ implies that $\vec{E}=0$ inside SC

Faradays Law

$$\oint \vec{E} \cdot d\vec{l} = - \frac{d\Phi}{dt}$$

Well inside SC $\vec{E}=0 \Rightarrow$

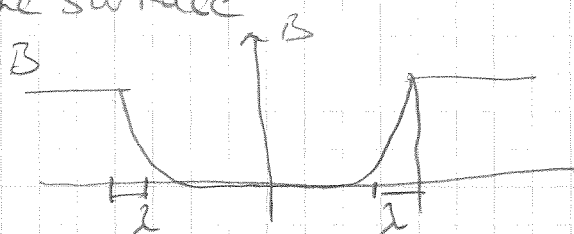
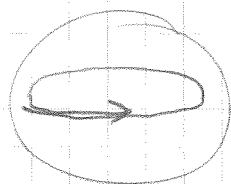
$$0 = - A \cdot \frac{dB}{dt} \Rightarrow \frac{dB}{dt} = 0$$

In fact $\vec{B} \equiv 0$ inside for SC

$$\vec{B} = \mu_0 (\vec{H} + \vec{M}) = \mu_0 (1 + \chi) \vec{H}$$

$\vec{B}=0 \Rightarrow \chi = -1$ ie perfect diamagnet

Screening currents at the surface



$$B = B_0 \cdot e^{-\frac{x}{\lambda}}$$

$$J_s = J_{s0} e^{-\frac{x}{\lambda}}$$

λ = London's penetration depth

$\sim 50 \text{ nm}$

DEMONSTRATION

The thermodynamic critical field

The Helmholtz Free energy (per unit volume)

$$F = E - TS - \mu_0 \bar{M} \cdot \bar{H}$$

$$dF = -SdT - \mu_0 \bar{M} d\bar{H}$$

$$F(H, T) = F(0, T) - \mu_0 \int_0^H \bar{M} d\bar{H}$$

Normal Metal, negligible magnetization

$$F(H, T) = F(0, T) \equiv F_N(T)$$

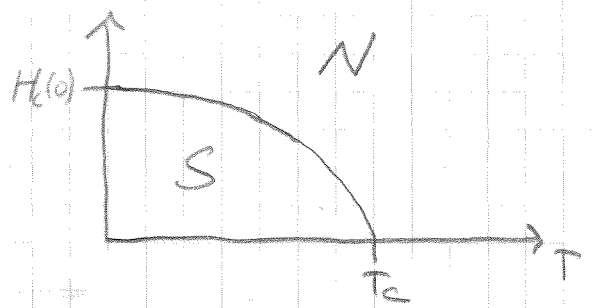
Superconductor $\chi = -1 \Rightarrow \bar{M} = -\bar{H}$ (Type I)

$$\begin{aligned} F_S(H, T) &= F_S(0, T) + \int_0^H H' dH' \\ &= F_S(0, T) + \frac{H^2}{2\mu_0} \end{aligned}$$

At the critical field H_c $F_N(T) = F_S(H_c, T)$

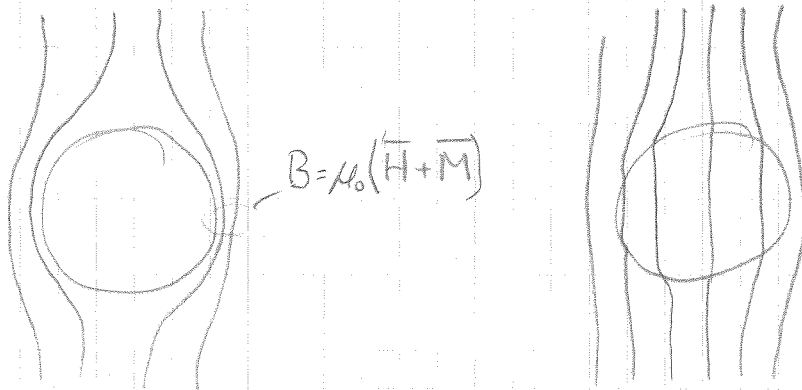
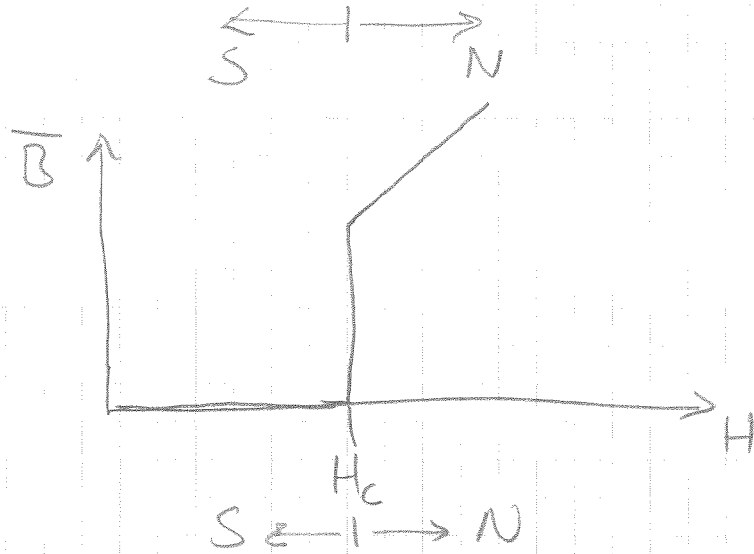
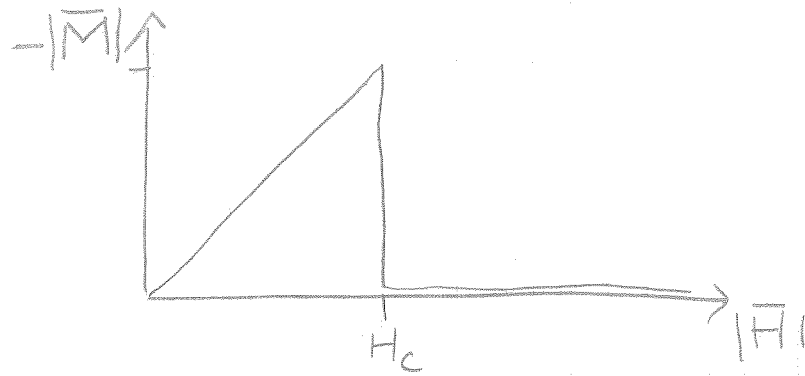
$$\Delta F = F_N(T) - F_S(H_c, T) = \frac{\mu_0}{2} H_c^2(T)$$

$$H_c(T) = H_c(0) \left[1 - \frac{T^2}{T_c^2} \right]$$



Type I SC in a magnetic field

Diamagnetism $\bar{M} = -\bar{H}$



$$H < \frac{2}{3} H_c$$

$$\frac{2}{3} H_c < H < H_c$$

If $H > \frac{2}{3} H_c$ then $H+M$ at the surface will be larger than H_c which will then the SC normal and flux will enter

Maxwells Equations

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{j} + \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t} \underset{\text{outside}}{=} 0$$

$$\vec{B} = \mu_0 \vec{H} \quad r \rightarrow \infty$$

Meissner no field lines enter the SC

$$\Rightarrow \vec{B}_n = 0 \quad r = a$$

Solution (using spherical coordinates)

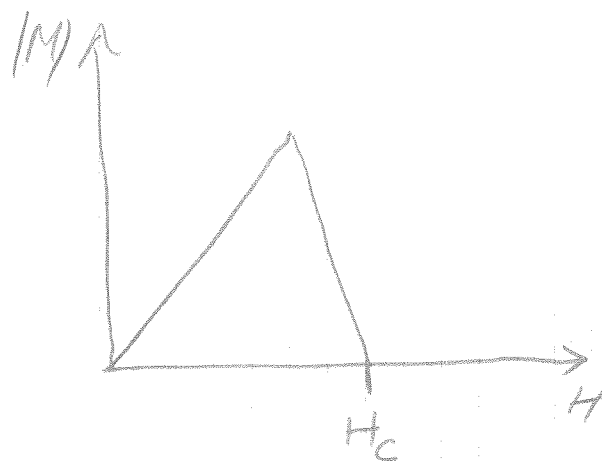
$$\vec{B} = \mu_0 \vec{H} + \mu_0 H \frac{a^3}{2} \nabla \left(\frac{\cos \theta}{r^2} \right)$$

$$\Rightarrow B_{||} = \frac{3}{2} \mu_0 H \cdot \sin^2 \theta$$

$$B_{|| \text{ max}} = \frac{3}{2} \mu_0 H$$

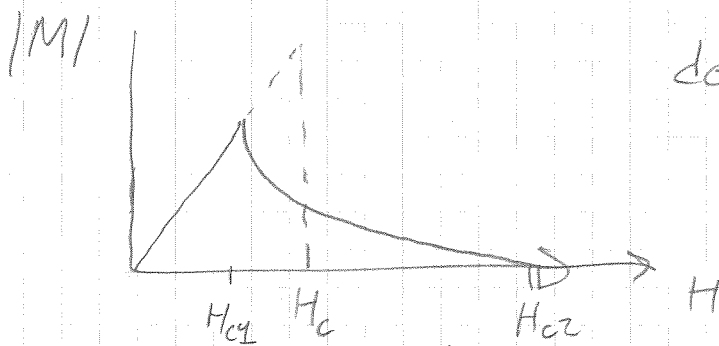
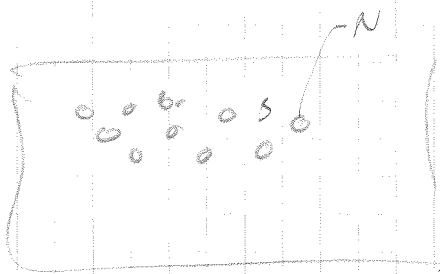
$$H = \frac{2}{3} H_c \quad \text{something will happen}$$

the intermediate state



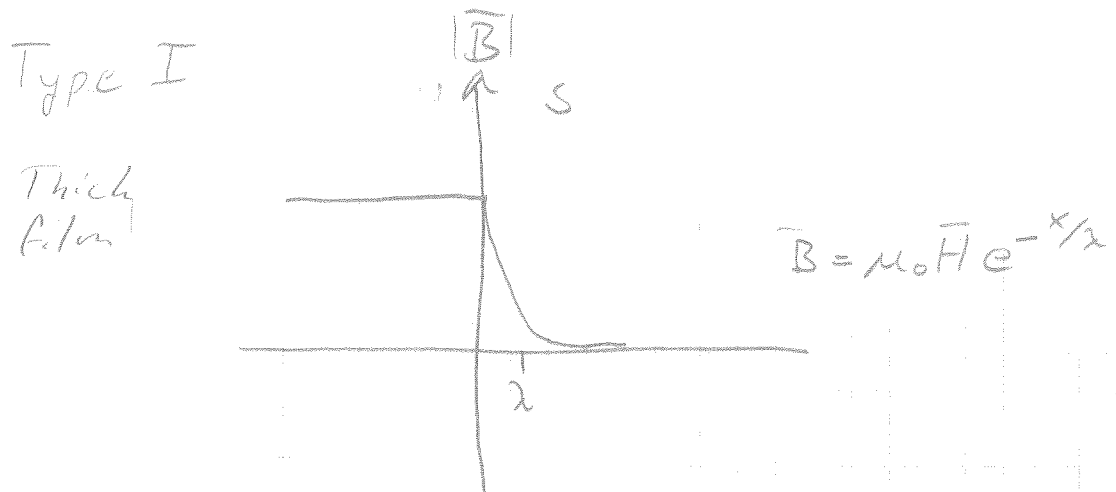
For type I SC the interface energy is positive, i.e. the SC tries to minimize the number of interfaces

For Type II the interface energy is negative as the SC tries to maximize the number of interfaces

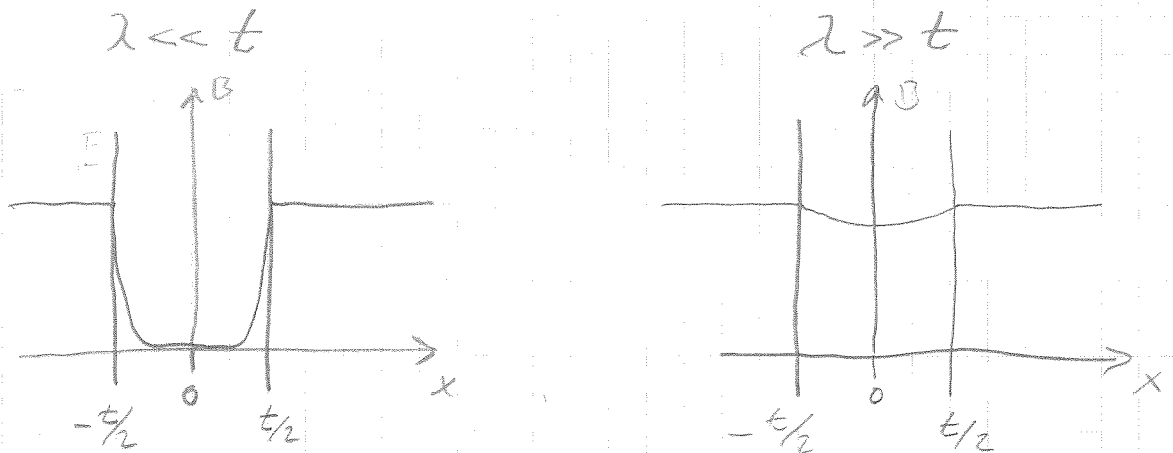


depends on κ

Enhancement of H_c in thin films



Thin film



$$\vec{B} = \mu_0 \vec{H} \cdot \frac{\cosh \frac{x}{\lambda}}{\cosh \frac{t}{2\lambda}}$$

$$\vec{M} = \frac{\vec{B}}{\mu_0} - \vec{H} = \vec{H} \left(\frac{\cosh \frac{x}{\lambda}}{\cosh \frac{t}{2\lambda}} - 1 \right)$$

$$M_{av} = \frac{1}{V} \int dV \vec{M} = \frac{1}{t} \int_{-t/2}^{t/2} dx M(x) =$$

$$= H \frac{1}{t} \int_{-t/2}^{t/2} \left(\frac{\cosh \frac{x}{\lambda}}{\cosh \frac{t}{2\lambda}} - 1 \right) dx = H \cdot \frac{1}{t} \left[\lambda \frac{\sinh \frac{x}{\lambda}}{\cosh \frac{t}{2\lambda}} - x \right]_{-t/2}^{t/2}$$

$$= H \frac{1}{t} \left[\lambda \tanh \frac{t}{2\lambda} - \frac{t}{2} - \tanh \left(\frac{t}{2\lambda} \right) + \left(-\frac{t}{2} \right) \right]$$

$$\tanh(-x) = -\tanh(x)$$

$$M_{av} = H \left[\frac{2i}{t} \tanh \frac{t}{2\lambda} - 1 \right]$$

$$\Delta F = -\mu_0 \int_0^H M_{av} \cdot dH'$$

$$= \frac{\mu_0}{2} H^2 \left[1 - \frac{2\lambda}{t} \tanh \left(\frac{t}{2\lambda} \right) \right]$$

$$\Delta F_{FF} = \Delta F_{Bulk} \Rightarrow$$

$$\frac{\mu_0}{2} H_c^{TF^2} \left[1 - \frac{2\lambda}{t} \tanh \left(\frac{t}{2\lambda} \right) \right] = \frac{\mu_0}{2} H_c^2$$

$$\frac{1}{x} \tanh x \approx \frac{1}{2} \left(x - \frac{x^3}{3} \dots \right) = 1 - \frac{x^2}{3}$$

$$H_c^{TF} = H_c \frac{1}{\sqrt{1 - \frac{2\lambda}{t} \tanh \left(\frac{t}{2\lambda} \right)}} \approx H_c \frac{1}{\sqrt{\frac{1}{3} \left(\frac{t}{2\lambda} \right)^2}}$$

$$H_c^{TF} = H_c^{Bulk} \sqrt{12} \frac{\lambda}{t}$$

$$GL \Rightarrow H_c^{TF} = H_c \sqrt{24} \frac{\lambda}{t}$$

Example Al 20nm thick

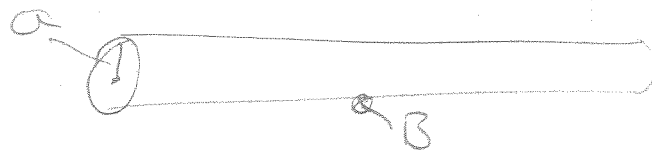
$$\lambda = 50 \text{ nm}$$

$$H_c^{TF} = H_c \cdot \sqrt{24} \frac{\lambda}{t} = H_c \cdot 12,2 \approx$$

$$1088 \cdot 12,2 \approx 1320 \text{ G} = 0,13 \text{ T}$$

Critical current of a SC wire

The Silsbee criterion



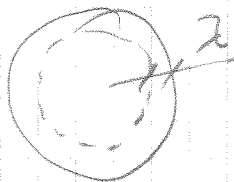
Biot-Savart

$$B = \frac{\mu_0}{4\pi} \frac{2I}{r} = \frac{\mu_0}{2\pi} \frac{I}{a}$$

$$B_c = \frac{\mu_0}{2\pi} \frac{I_c}{a} = \mu_0 H_c$$

$$I_c = \underbrace{2\pi a}_{\text{circumference}} \cdot H_c$$

"thick wire"
 $a \gg \lambda$



$$J_c = \frac{I_c}{A} = \frac{I_c}{2\pi a \cdot \lambda} = \frac{H_c}{\lambda}$$

$$J_c = \frac{H_c}{\lambda}$$

$$I_c = 2\pi a H_c$$